

Complementary note on:  
**Solution of a first-order differential equation  
with decaying *gain***

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**Abstract**

This note aims at complementing the formal analysis provided in papers [1] and [2] in relation to terminal convergence of a first-order differential equation with decaying *gain*. Considerations included in this note leads to the correction of an improper corollary formulated in [2] with respect to equation<sup>1</sup> {31}.

## 1 General considerations

Let us consider the first-order differential equation of the form

$$\dot{x}(t) = -cg(t) \sin x(t), \quad (1)$$

where  $c > 0$  is a positive constant,  $t$  is time variable, and  $g(t)$  is a bounded nonnegative function such that  $g(t) \rightarrow 0$  as  $t \rightarrow \infty$ . The term  $cg(t)$  will be called the *gain*, which in our case terminally tends to zero (decays). Solution of (1) for  $x \in [-\pi, \pi]$  can be written as

$$x(t) = 2 \arctan [X_0 \cdot \exp(-cI(0,t))], \quad t \geq 0, \quad (2)$$

where  $X_0 = \tan \frac{x(0)}{2}$ , and

$$I(0,t) \triangleq \int_0^t g(\xi) d\xi. \quad (3)$$

We are interested in the terminal behavior of solution (2) as  $t \rightarrow \infty$ . It directly depends on integral (3) evaluated in infinity, namely  $I(0,\infty)$ . The terminal convergence of  $x(t)$  to zero (for  $t \rightarrow \infty$ ) requires  $I(0,\infty) = \infty$ , which could be obtained for instance if  $g(t) = g = \text{const}$ . But it is not the case here, since we assume  $g(t) \rightarrow 0$ . The fact that  $g(t \rightarrow \infty) \rightarrow 0$  does not necessarily preclude convergence of  $x(t)$  to zero. It depends of the rate of convergence of function  $g(t)$ . Thus, to make an appropriate conclusion about terminal behavior of  $x(t)$  one has to investigate integrability of function  $g(t)$ .

## 2 Application of the above result to papers [2] and [1]

In paper [2], equation {31} is in the form of (1) by taking  $x := e_\theta$ ,  $c := -\text{sgn}(e_{x0})/L_1$ , and  $g(t) := \|\mathbf{h}^*(t)\|$ . To check if the error  $e_\theta(t)$  terminally converges to zero we must investigate integrability of  $\|\mathbf{h}^*(t)\|$  (according to the result (2)-(3)). Recalling the results presented in [2] we know that  $\mathbf{h}^* = \mathbf{h}^*(t) = k_p \mathbf{e}^*(t) - \eta \sigma \|\mathbf{e}^*(t)\| \mathbf{g}_2^*(\beta_t)$ , thus (note:  $\|\mathbf{g}_2^*(\beta_t)\| \equiv 1$  and  $\sigma \in \{-1, +1\}$ )

$$\|\mathbf{h}^*(t)\| \leq (k_p + \eta) \|\mathbf{e}^*(t)\| = b \|\mathbf{e}^*(t)\|, \quad \eta \in (0, k_p). \quad (4)$$

Since  $b = (k_p + \eta) > 0$  is a constant, integrability of  $\|\mathbf{h}^*(t)\|$  is equivalent to integrability of  $\|\mathbf{e}^*(t)\|$ . According to the results presented in [3] (cf. page 53), for the set-point control task with the VFO controller one can write

$$I(0,\infty) = \int_0^\infty \|\mathbf{h}^*(t)\| dt \\ \leq b \int_0^\infty \|\mathbf{e}^*(t)\| dt = b \int_0^{\tau_\gamma} \|\mathbf{e}^*(t)\| dt + b \int_{\tau_\gamma}^\infty \|\mathbf{e}^*(t)\| dt \leq E_\gamma + b \int_{\tau_\gamma}^\infty \|\mathbf{e}^*(\tau_\gamma)\| \exp(-\zeta_\gamma(t - \tau_\gamma)) dt, \quad (5)$$

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<sup>1</sup>References to particular equations taken from papers [1-3] are indicated by numbers in {·} brackets.

where  $0 \leq E_\gamma < \infty$ ,  $\tau_\gamma \geq 0$ ,  $\zeta_\gamma > 0$ , and  $\|\mathbf{e}^*(\tau_\gamma)\| < \infty$ . As a consequence, integral (5) is bounded, since

$$I(0, \infty) \leq E_\gamma + b \|\mathbf{e}^*(\tau_\gamma)\| / \zeta_\gamma. \quad (6)$$

Hence, one concludes that  $I(0, \infty) < \infty$ , and error  $e_\theta(t)$  terminally **does not converge to zero** – in contrast to the incorrect statement about *local asymptotic stability of equilibrium*  $e_{\theta 1E} = 0$  formulated in [2] on page 270 under equation {31}. Terminal value of  $e_\theta$  depends on the value of integral (3) at infinity (for  $t \rightarrow \infty$ ).

Similar arguments apply to the analysis done in paper [1] on page 512 where the integral defined by {64} has been considered (cf. also Remark 2 on page 512). Upon {64} one can write<sup>2</sup>

$$\begin{aligned} I(\tau_d, \tau) &= \int_{\tau_d}^{\tau} s(\xi) \|\mathbf{h}^*(\bar{\mathbf{e}}(\xi))\| \cos e_a(\xi) d\xi \leq \int_{\tau_d}^{\tau} \|\mathbf{h}^*(\bar{\mathbf{e}}(\xi))\| d\xi \\ &\leq \int_{\tau_d}^{\tau} (k_p + \eta) \|\bar{\mathbf{e}}^*(\xi)\| d\xi = (k_p + \eta) \int_{\tau_d}^{\tau} \|\bar{\mathbf{e}}^*(\xi)\| d\xi, \end{aligned} \quad (7)$$

where we have used the fact that  $\|\mathbf{h}^*(\bar{\mathbf{e}}(t))\|$  satisfies analogous relation to (4), and  $\forall \tau \geq 0$   $s(\tau) \in (0, 1]$ . The right-hand side of (7) is finite for any  $\tau < \infty$ . Furthermore, for the asymptotic case with  $\delta = 0$  taken in {17} one should consider now the integral at infinity

$$I(\tau_d, \infty) \leq (k_p + \eta) \int_{\tau_d}^{\infty} \|\bar{\mathbf{e}}^*(\xi)\| d\xi < \infty \quad (8)$$

which is finite by referring to similar reasoning as in (5)-(6). Hence, asymptotic convergence of joint angle (see Eq. {62})

$$\lim_{\tau \rightarrow \infty} \beta_N(\tau) = 2 \arctan \left( B_{Nd} \cdot \exp \left( \frac{\sigma}{L_{hN}} I(\tau_d, \infty) \right) \right), \quad (\sigma/L_{hN}) < 0 \quad (9)$$

to zero **is not possible** also in this case. However, according to (9) one may find that terminal value of  $\beta_N$  will be smaller for smaller value of offset  $|L_{hN}|$ . The above complementary analysis confirms and extends (for the case of  $\delta = 0$ ) the statements included in Remark 2 in [1].

## References

- [1] M. Michałek. Application of the VFO method to set-point control for the N-trailer vehicle with off-axle hitching. *International Journal of Control*, 85(5):502–521, 2012.
- [2] M. Michałek and K. Kozłowski. VFO tracking and set-point control for an articulated vehicle with off-axle hitched trailer. In *Proc. of the European Control Conference*, pages 266–271, Budapest, Hungary, 2009.
- [3] M. Michałek and K. Kozłowski. Vector-Field-Orientation feedback control method for a differentially driven vehicle. *IEEE Transactions on Control Systems Technology*, 18(1):45–65, 2010.

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<sup>2</sup>Henceforth, the notation and symbols are used according to [1].